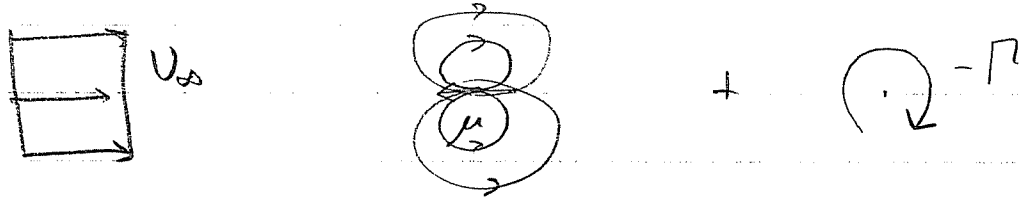


How to fly?

XI

Flow past a circular cylinder with circulation.



uniform
stream

doublet
 $\mu = 2\pi U_\infty a^2$

vortex

$$F(z) = U_\infty \left(z + \frac{a^2}{z} \right) + \frac{i\Gamma}{2\pi} \ln z, \quad z = re^{i\theta}$$

→

$$\Psi = U_\infty \sin\theta \left(r - \frac{a^2}{r} \right) + \frac{\Gamma}{2\pi} \ln(r/a)$$

$r = a \Rightarrow \Psi = 0 \therefore$ streamline

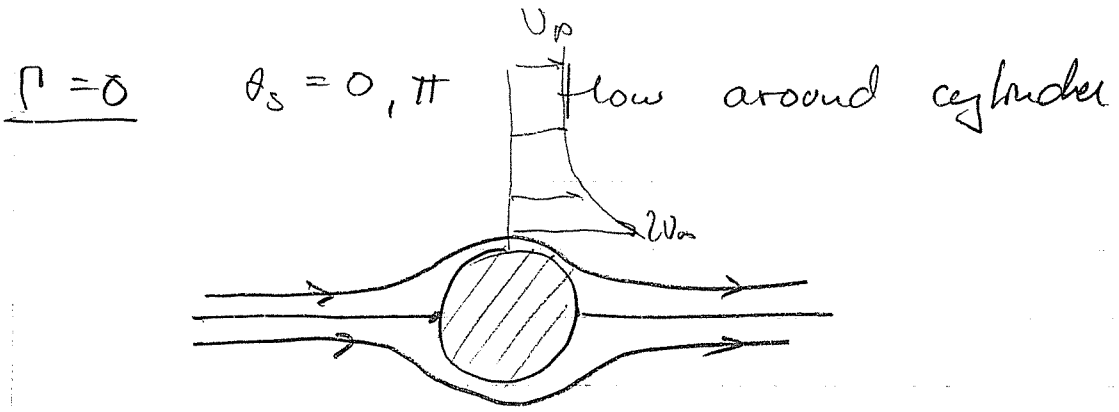
Complex velocity

$$\begin{aligned} W = F'(z) &= U_\infty \left(1 - \frac{a^2}{z^2} \right) + \frac{i\Gamma}{2\pi z} = \dots = \\ &= \underbrace{\left\{ U_\infty \left(1 - \frac{a^2}{r^2} \right) \cos\theta \right\}}_{= u_r} + i \underbrace{\left\{ U_\infty \left(1 + \frac{a^2}{r^2} \right) \sin\theta + \frac{\Gamma}{2\pi r} \right\}}_{= -u_\theta} e^{-i\theta} \end{aligned}$$

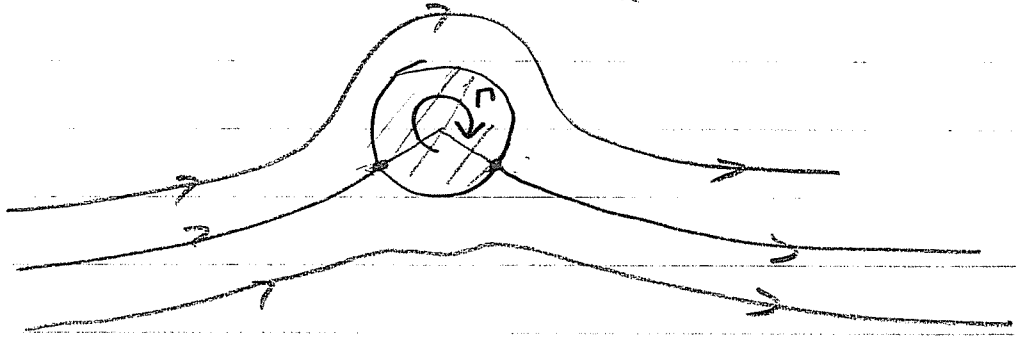
Stagnation points: $u_r = 0 \Rightarrow r = a$

$$u_\theta = -2U_\infty \sin\theta_s - \frac{\Gamma}{2\pi a} = 0$$

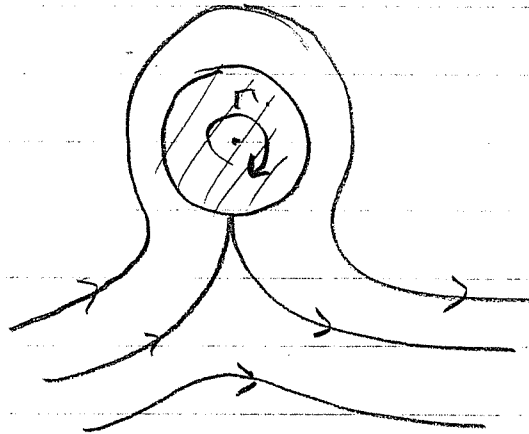
$$\Rightarrow \sin\theta_s = -\frac{\Gamma}{4\pi a U_\infty} \quad \text{or if } \Gamma < 4\pi a U_\infty$$



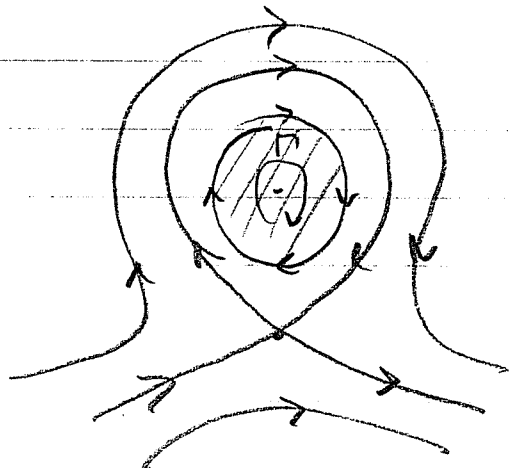
$\Gamma < 4\pi a U_\infty$ $\theta_s = -\underbrace{\arcsin \Gamma / 4\pi a U_\infty}_\alpha, \pi + \arcsin \Gamma / 4\pi a U_\infty$



$\Gamma = 4\pi a U_\infty$



$\Gamma > 4\pi a U_\infty$



Pressure on cylinder surface

Bernoulli's eq. $\Rightarrow p(\theta) + \frac{1}{2} \rho U_{\theta}^2(r=a, \theta) = P_{\infty} + \frac{1}{2} \rho U_{\infty}^2$

$$U_{\theta}^2(r=a, \theta) = \left(-2U_{\infty} \sin \theta - \frac{\Gamma}{2\pi a} \right)^2 = 4U_{\infty}^2 \left(\sin \theta + \sin \alpha \right)^2$$

$$= 4U_{\infty}^2 \sin^2 \theta + 4U_{\infty}^2 \sin^2 \alpha + 8U_{\infty}^2 \sin \theta \sin \alpha$$

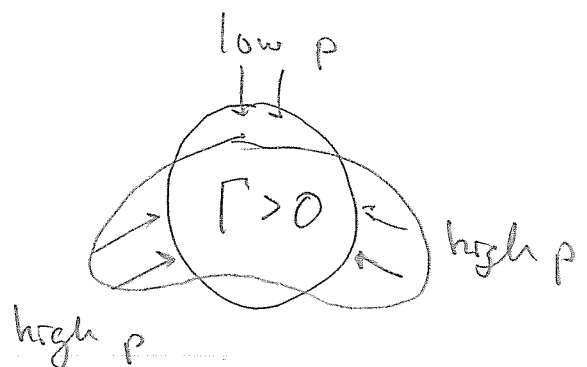
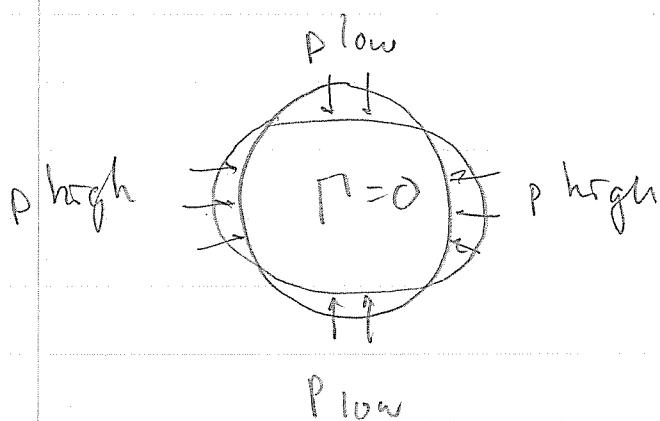
Pressure coefficient $C_p \hat{=} \frac{p - P_{\infty}}{\frac{1}{2} \rho U_{\infty}^2} =$

$$= 1 - 4 \sin^2 \theta - 4 \sin^2 \alpha - 8 \sin \theta \sin \alpha \quad \{ \text{see graph} \}$$

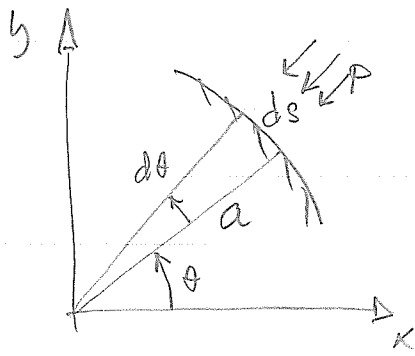
$$\sin \alpha = \frac{\Gamma}{4\pi U_{\infty} a}$$

$\Gamma = 0 \Rightarrow \sin \alpha = 0$ symmetric pressure distribution
no lift force, no drag force

$\Gamma > 0 \Rightarrow \sin \alpha > 0$ lift force > 0 , drag force $= 0$



Calculation of lift



$$dL'_y = -\rho(n=a) \frac{a d\theta \sin \theta}{ds}$$

$$L'_y = \int_0^{2\pi} dL'_y = \dots = \frac{1}{2} \rho U_\infty^2 a \int_0^{2\pi} (-c_p) \sin \theta d\theta =$$

$$= \left\{ \int_0^{2\pi} \sin^2 \theta d\theta = \pi, \text{ others} = 0 \right\} =$$

$$= \frac{1}{2} \rho U_\infty^2 a \delta \pi \sin \alpha$$

$$C'_L = \frac{L'_y}{\frac{1}{2} \rho U_\infty^2 \cdot 2a} = 4\pi \sin \alpha$$

"angle of attack"

$$L'_y = \frac{1}{2} \rho U_\infty^2 a \delta \pi \frac{\Gamma}{4\pi U_\infty a} = \frac{\rho \Gamma U_\infty}{\uparrow}$$

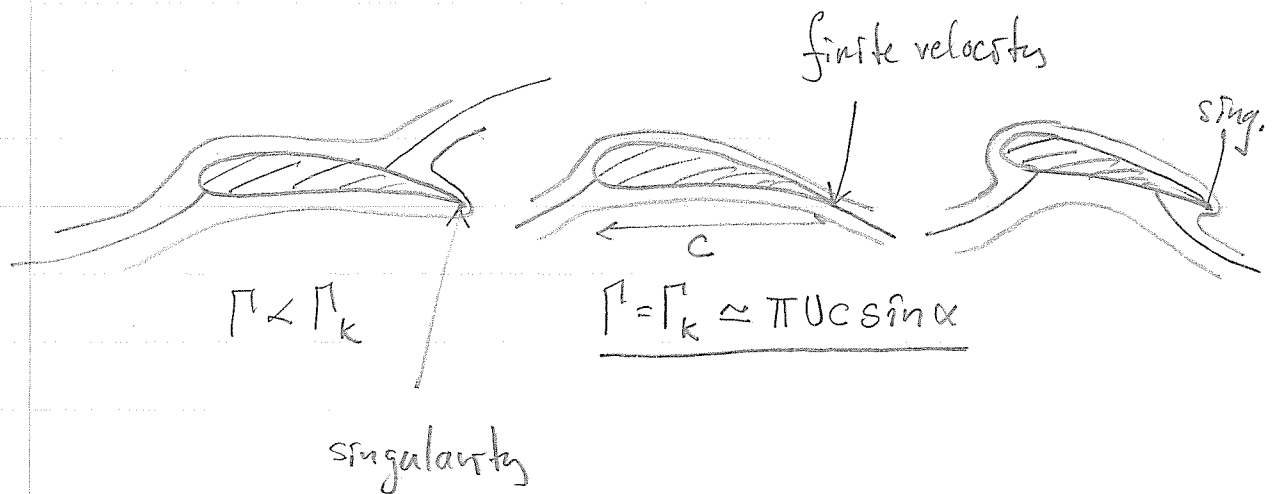
proportional to
circulation

Kutta-Joukowski lift theorem

Result for circular cylinder holds for any cylinder shape

$$\text{drag } D' = 0, \text{ lift } L' = \rho \Gamma U_\infty$$

Γ is determined by the shape of the cylinder



Kutta condition on circulation gives finite velocity at rear edge.

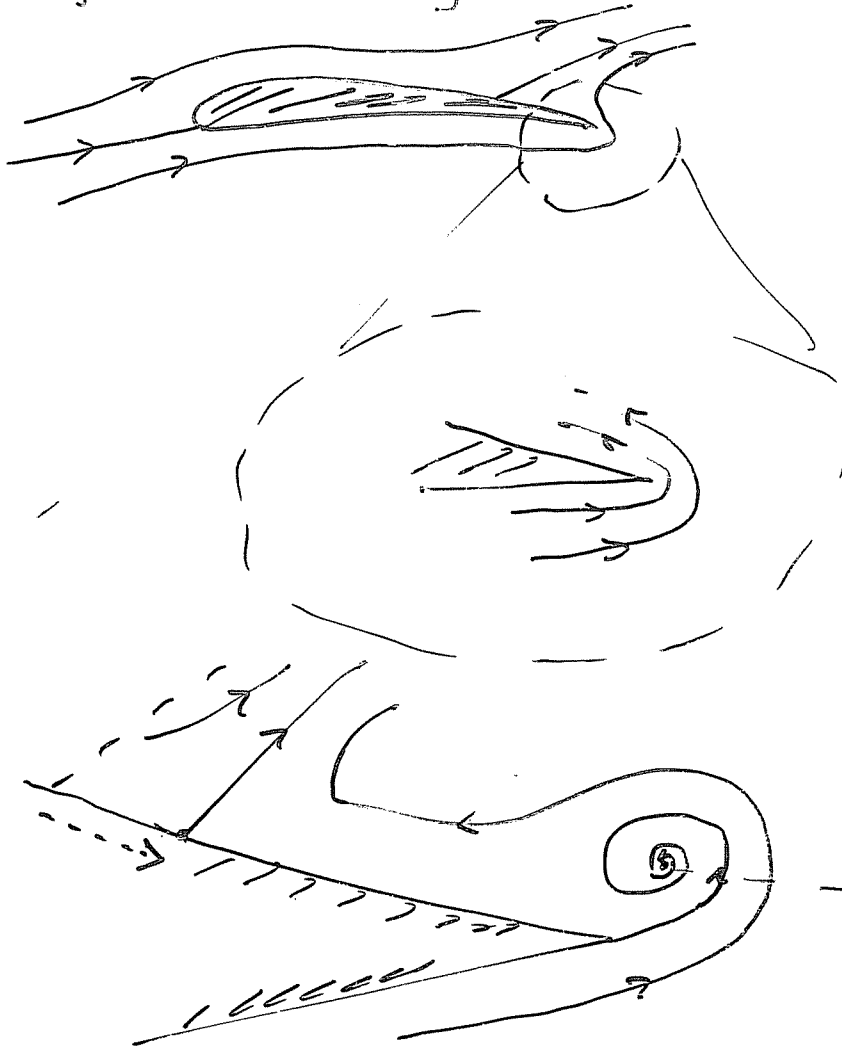
In reality, the circulation is generated by vortex shedding as a result of viscous effects.

{ Show: Generation of circulation }

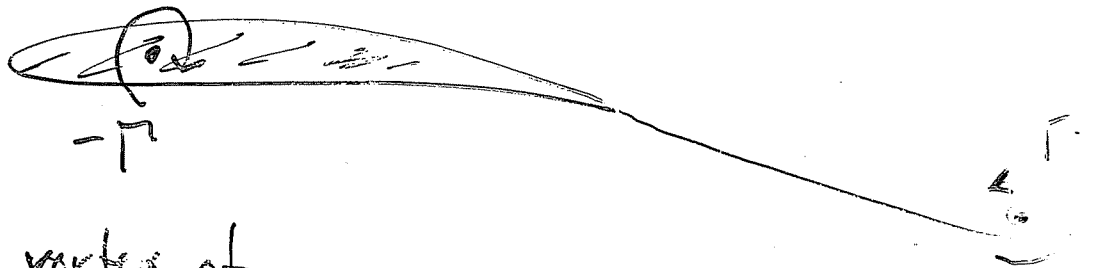
GENERATION OF CIRCULATION

Batchelor 1917
 An introduction
 to Fluid Dynamics

Recently started wing



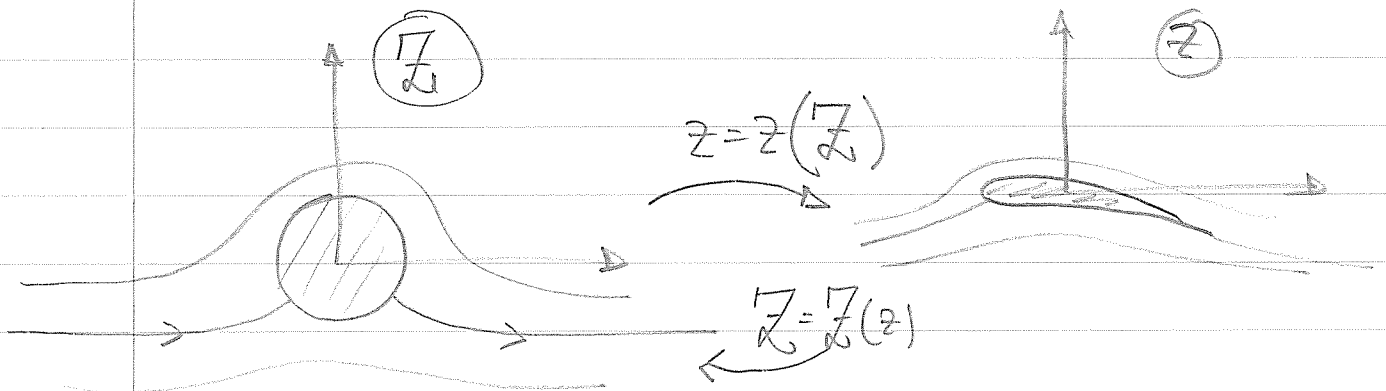
vorticity shed
 from boundary layer
 --- generates spiral
 vortex sheet of
 total circulation Γ



"mirror" vortex of
 circulation $-\Gamma$

Starting
 vortex
 Γ

Conformal mapping: Transforming one flow into another



Body of which you know $F(\zeta_1)$

Velocity potential for mapped body $F(z(z_1))$

Velocity around mapped body

$$u - iv = W(z) = \frac{dF}{dz} = \frac{dF}{d\zeta} \frac{d\zeta}{dz} = \frac{\frac{dF}{d\zeta}}{\frac{dz}{d\zeta}}$$

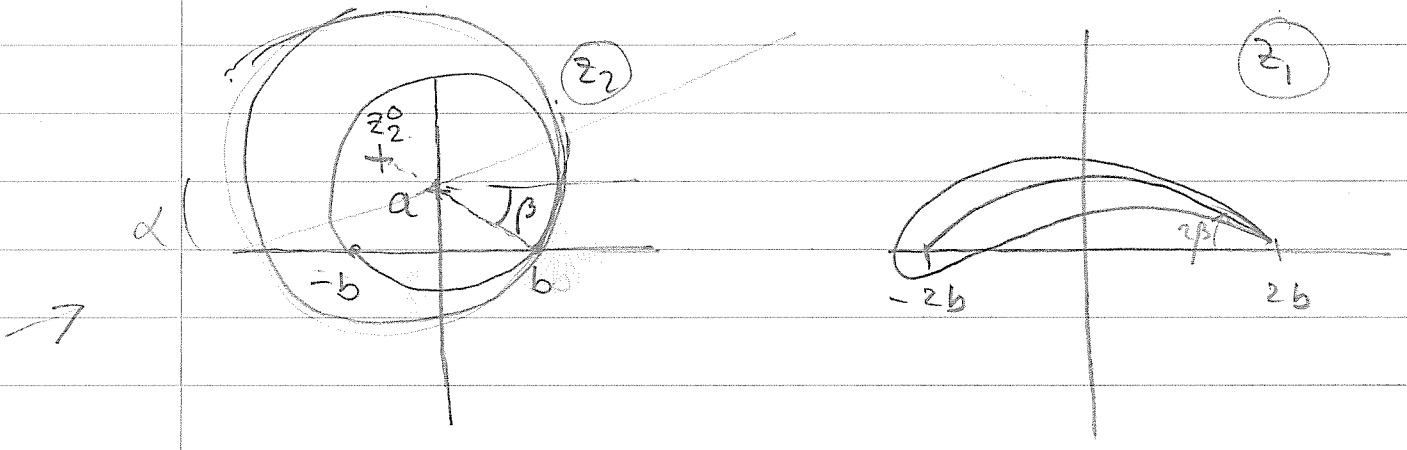
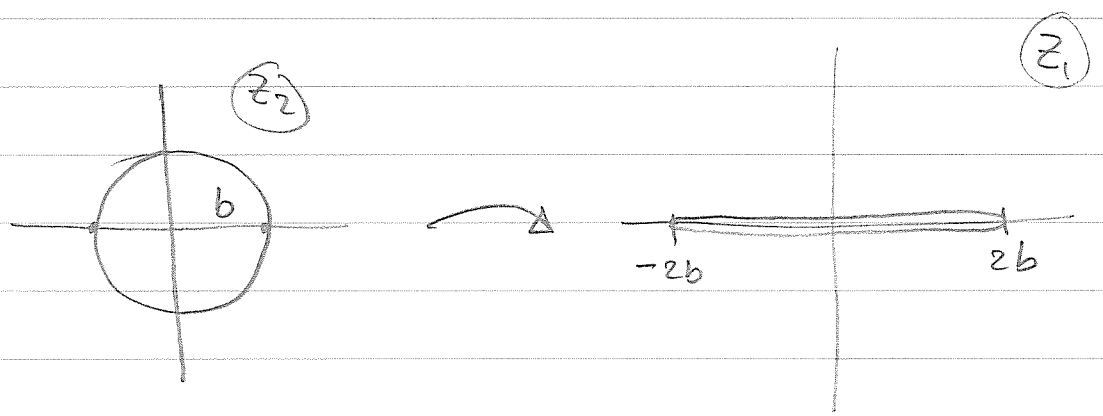
If $z(\zeta)$ and $F(\zeta)$ are analytic

then $F(z)$ is also analytic.

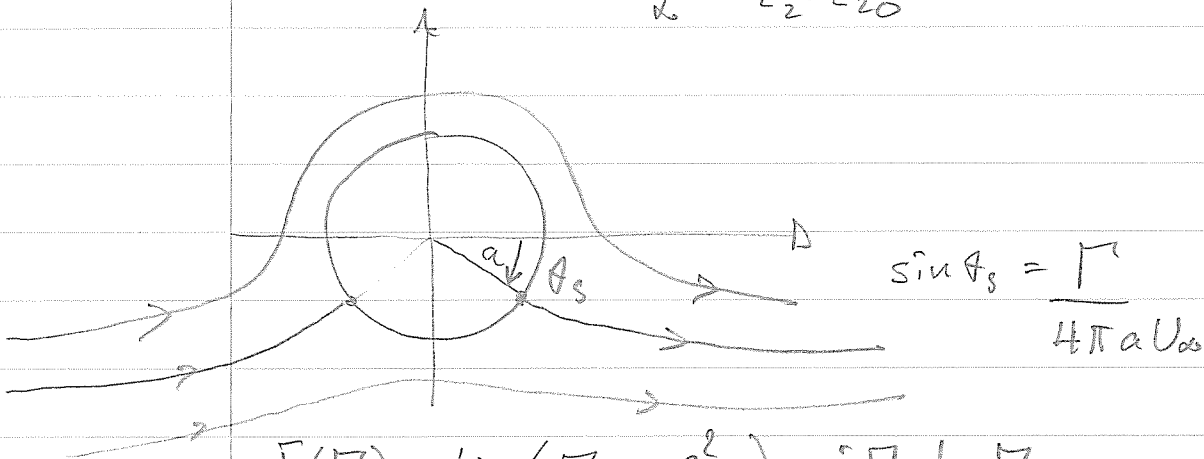
Study the transformation

$$z_1 = z_2 + \frac{b^2}{z_2} = b e^{i\theta_2} + \frac{b^2}{b e^{i\theta_2}} = b(e^{i\theta_2} + e^{-i\theta_2}) = 2b \cos \theta_2$$

circle in z_2 -plane: $z_2 = b e^{i\theta_2}$



$$\bar{z} = z_2 - z_{20}$$



$$\sin \theta_s = \frac{\Gamma}{4\pi a U_\infty}$$

$$F(\bar{z}) = U_\infty \left(\bar{z} + \frac{a^2}{\bar{z}} \right) + \frac{i\Gamma}{2\pi} \ln \frac{\bar{z}}{a}$$

Kutta condition: rear stagnation point must coincide with the trailing edge
i.e. $\theta_s = \beta$

$$\Rightarrow \sin \beta = \frac{\Gamma}{4\pi a U_\infty}$$

$$\text{Lift force } L' = \rho \Gamma U_\infty = \rho U_\infty^2 4\pi a \sin \beta$$

$$u - iv = \frac{dF}{dz_1} = \frac{dF}{d\bar{z}} \frac{d\bar{z}}{dz_1} =$$

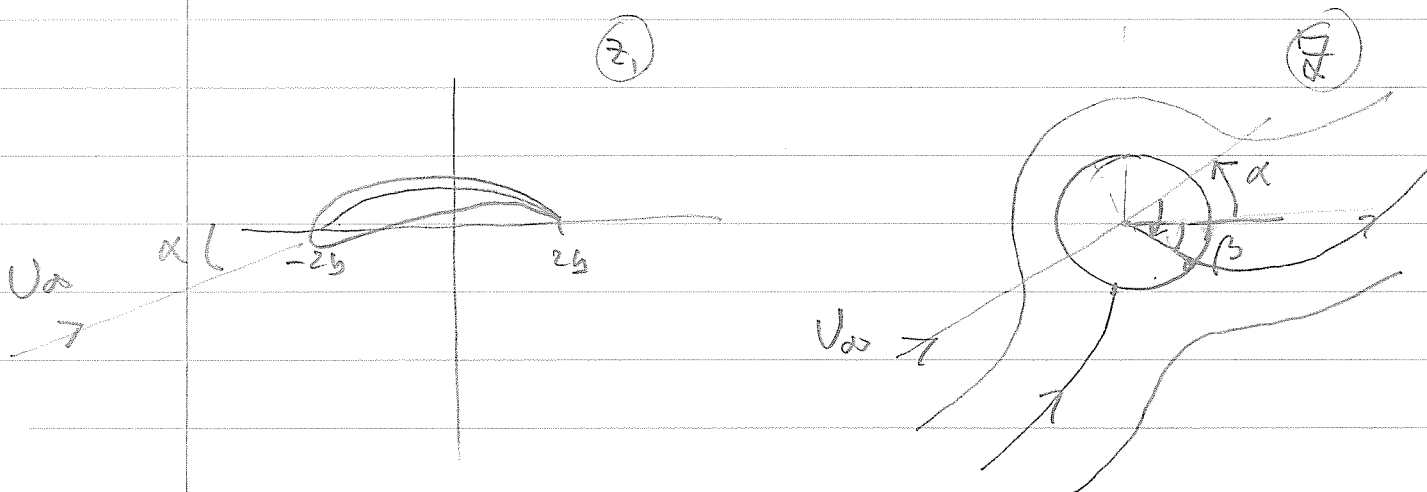
$$= \frac{dF}{d\bar{z}} \frac{d\bar{z}_1}{dz_2} \frac{dz_2}{d\bar{z}} = \frac{U_\infty \left(1 - \frac{a^2}{\bar{z}^2} \right) + \frac{i\Gamma}{2\pi} \frac{1}{\bar{z}}}{1 - b^2/\bar{z}^2}$$

$$\text{At trailing edge } z_2 = b \Rightarrow \frac{dF}{dz_1} \rightarrow \infty$$

$$\text{unless } \frac{dF}{d\bar{z}} = 0 \text{ at } \bar{z} = a e^{-i\beta},$$

OK, because of Kutta condition.

Angle of attack α :



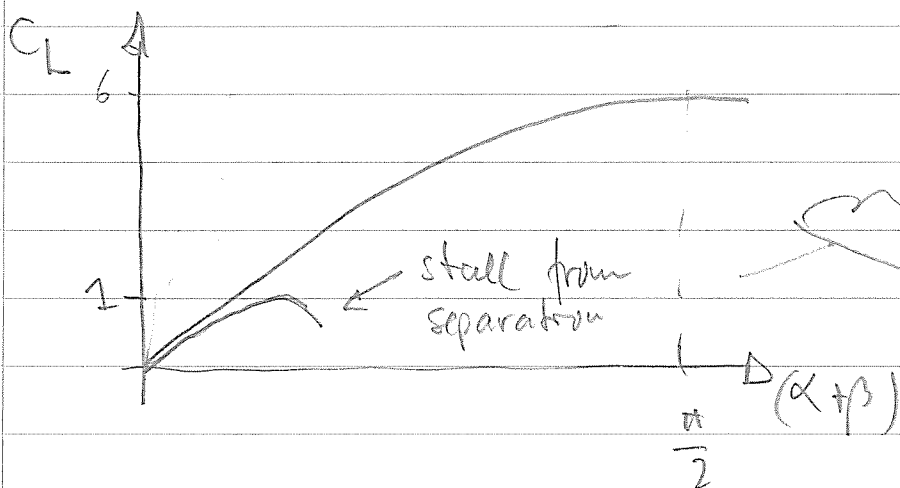
$$\Gamma_k = 4\pi a U_\infty \sin(\alpha + \beta)$$

$$L' = 2U_\infty^2 4\pi a \sin(\alpha + \beta)$$

Lift coefficient $C_L = \frac{L'}{\frac{1}{2}\rho U_\infty^2 c}$ $c \approx 4b$

$$= 2\pi \frac{a}{b} \sin(\alpha + \beta)$$

$$\left(a = \frac{(1+\epsilon)b}{\cos\beta} \Rightarrow C_L = 2\pi \frac{(1+\epsilon)}{\cos\beta} \sin(\alpha + \beta) \right)$$



[show OK]
[WACA 2018]